

## Session F (April 13, 2024) Saturday



A **transient theory** for solute transport through **redox flow battery** electrodes in the **creeping flow regime**



Md Abdul Hamid  
[mdabdul2@illinois.edu](mailto:mdabdul2@illinois.edu)

Kyle C. Smith  
[kcsmith@illinois.edu](mailto:kcsmith@illinois.edu)

University of Illinois at Urbana-Champaign  
Department of Mechanical Science and Engineering, Urbana, IL, USA 61801

# Introduction

## What are batteries ???



# Introduction

## What are flow batteries ???

Turlock, CA



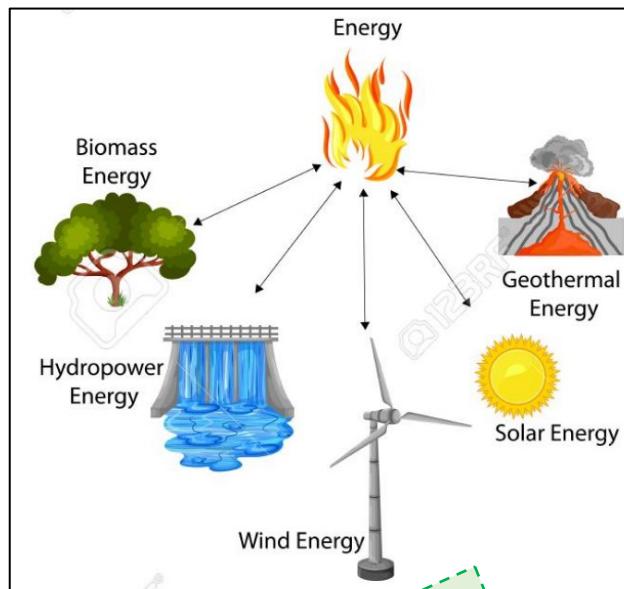
EnerVault deploys grid-scale redox flow battery for energy storage.

Central Valley, California. June-2014

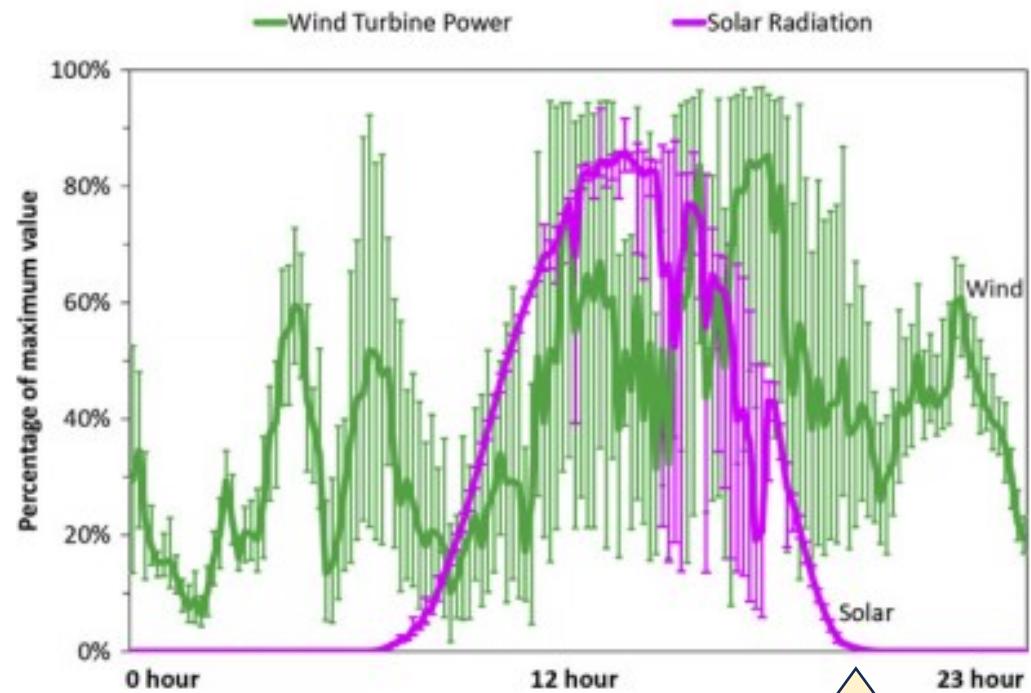
<https://worldindustrialreporter.com/redox-flow-battery-connects-solar-grid/>

# Introduction

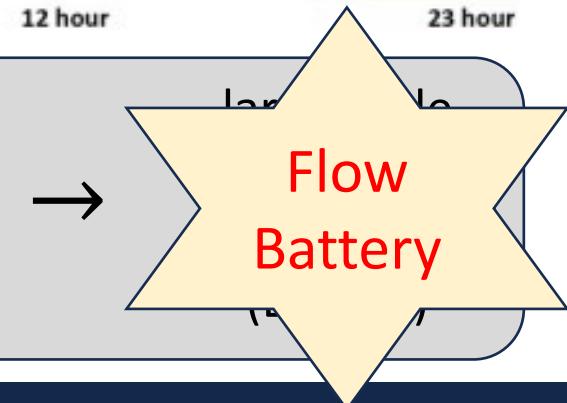
## What do we want to do with flow batteries ???



Power from  
**renewable**  
sources.

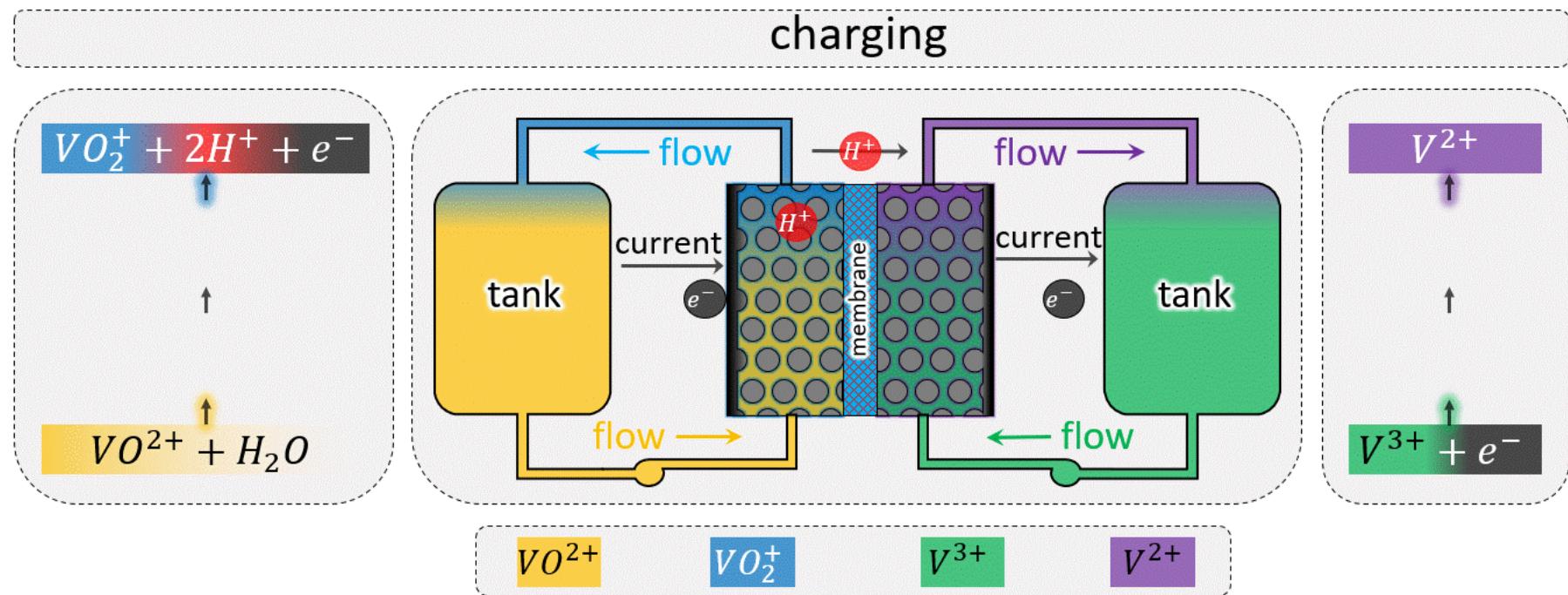


intermittent  
supply and  
demand



# Introduction

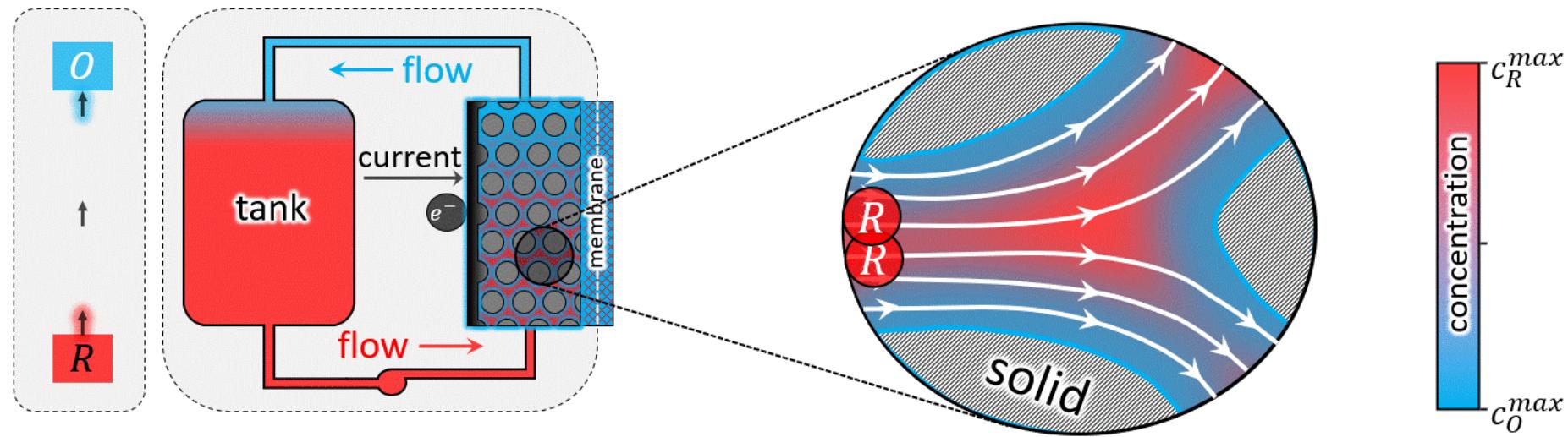
## How does a flow battery work ???



Two symmetric-separated halves

# Introduction

## More detailed look inside porous electrode



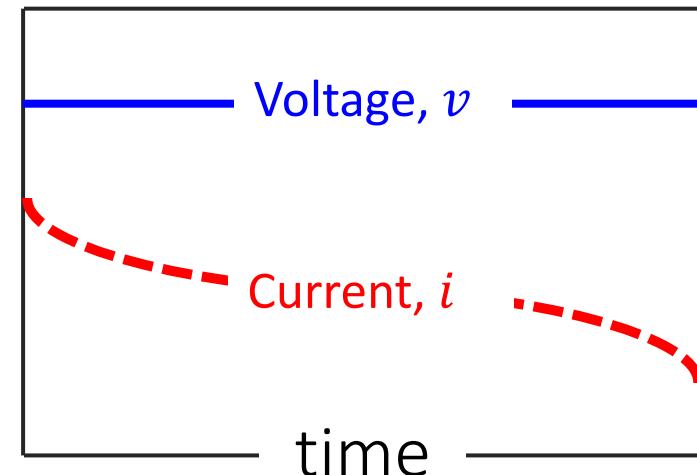
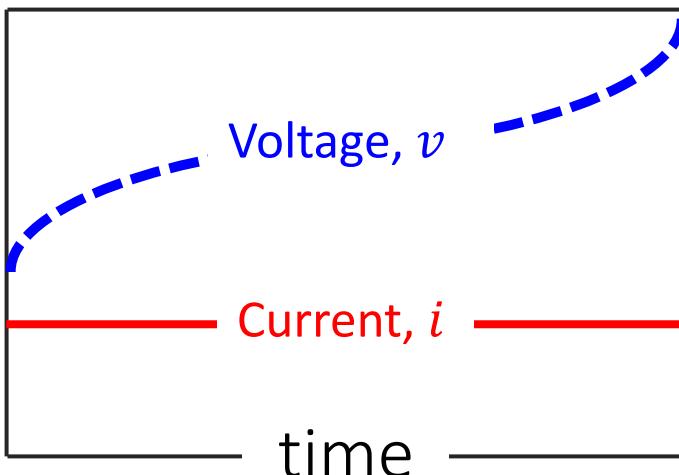
Half-cell with  
oxidation reaction

Reaction, advection  
and diffusion

# Simplest experiment with battery

What would you do if:

You are **given a battery** & you are told to **collect some data**



Measure voltage

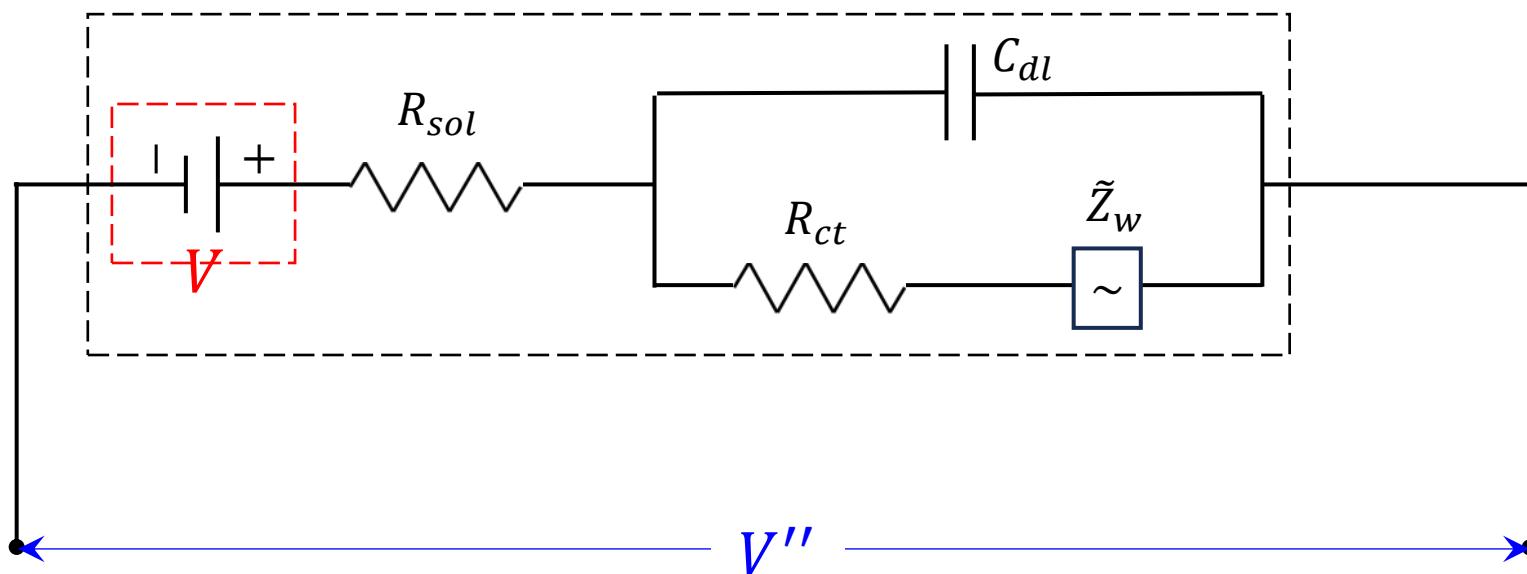
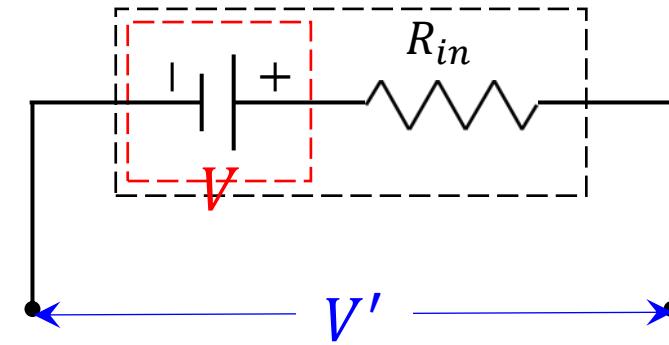
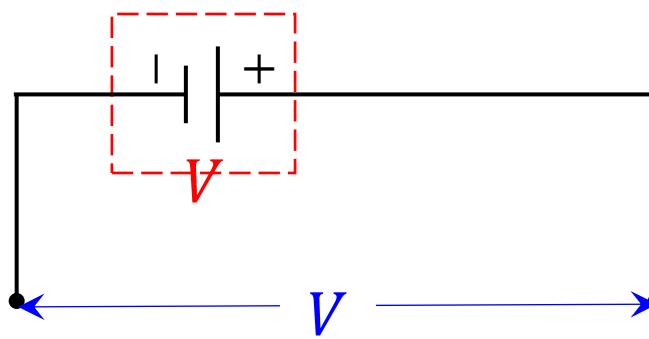
Control current

Control Voltage

Measure current

$$Z_{eq}(t)$$

# Equivalent circuit models

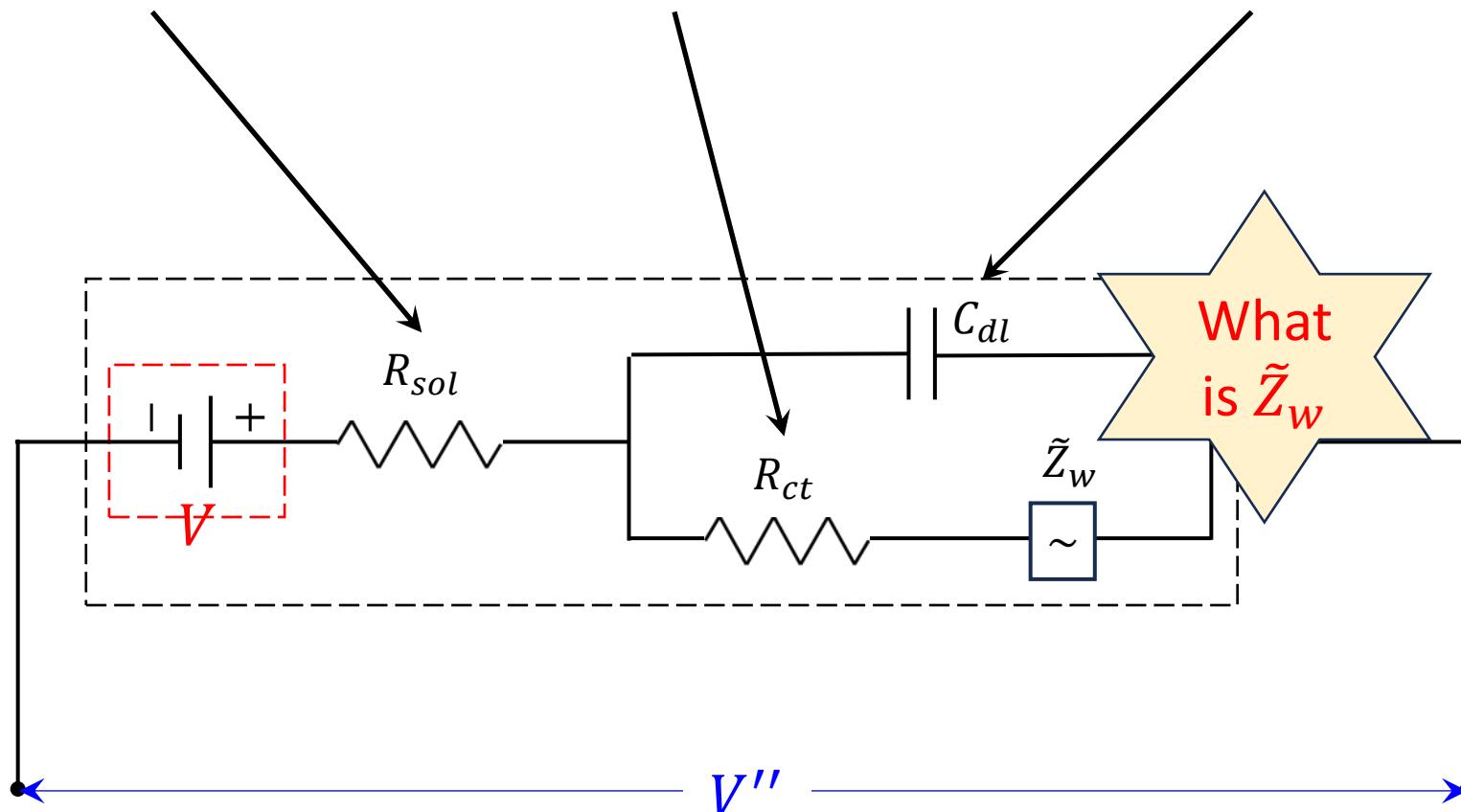


# Warburg impedance

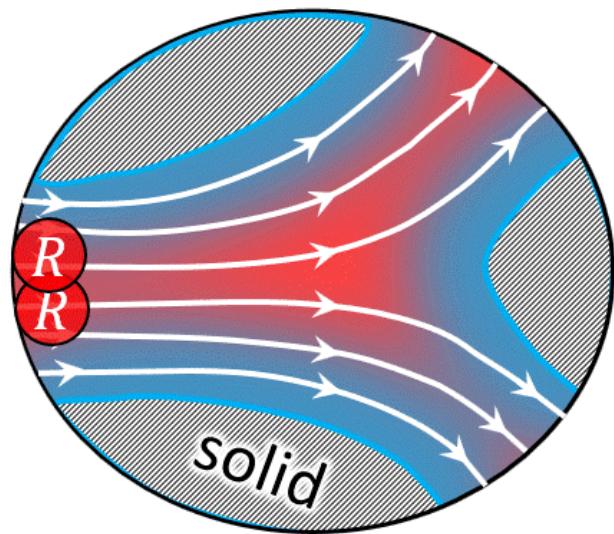
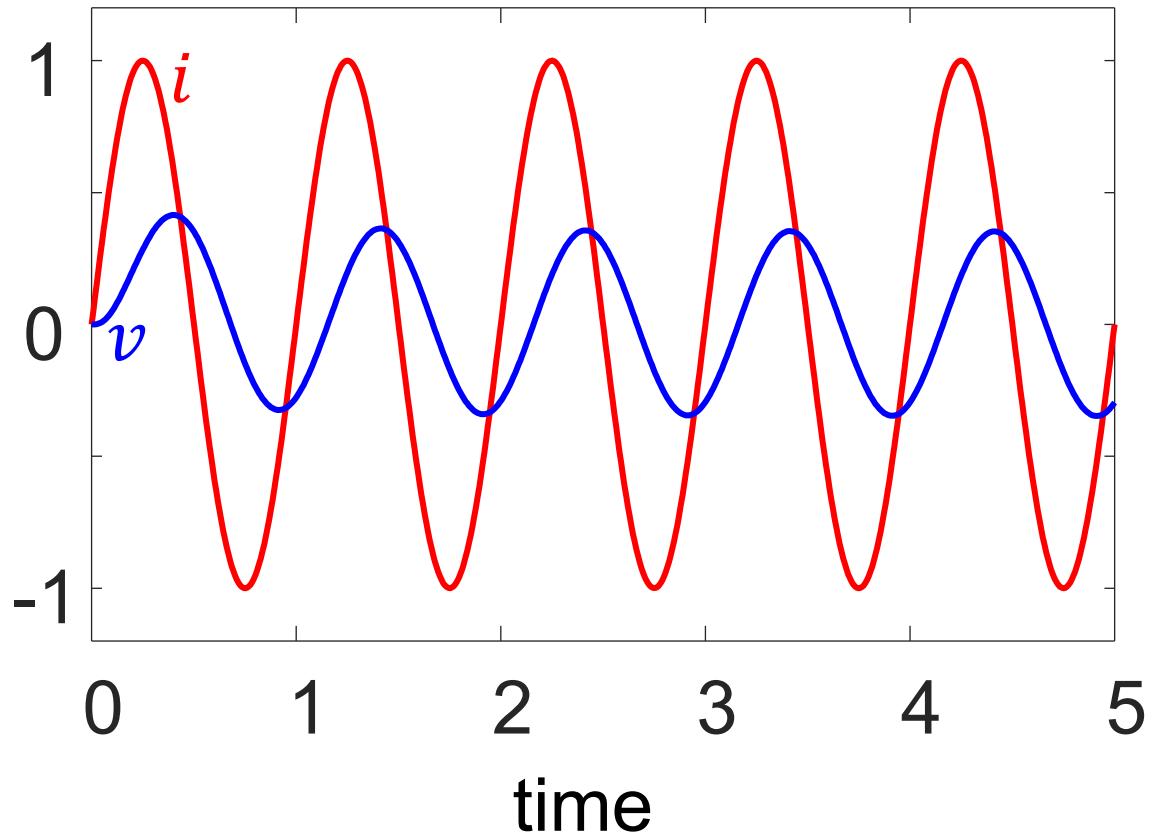
Sufficient supporting salt,  
negligible  $R_{sol}$

Fast reaction kinetics,  
Negligible  $R_{ct}$

Current variation frequency  $\ll MHz$ ,  
Effect of  $C_{dl}$  negligible



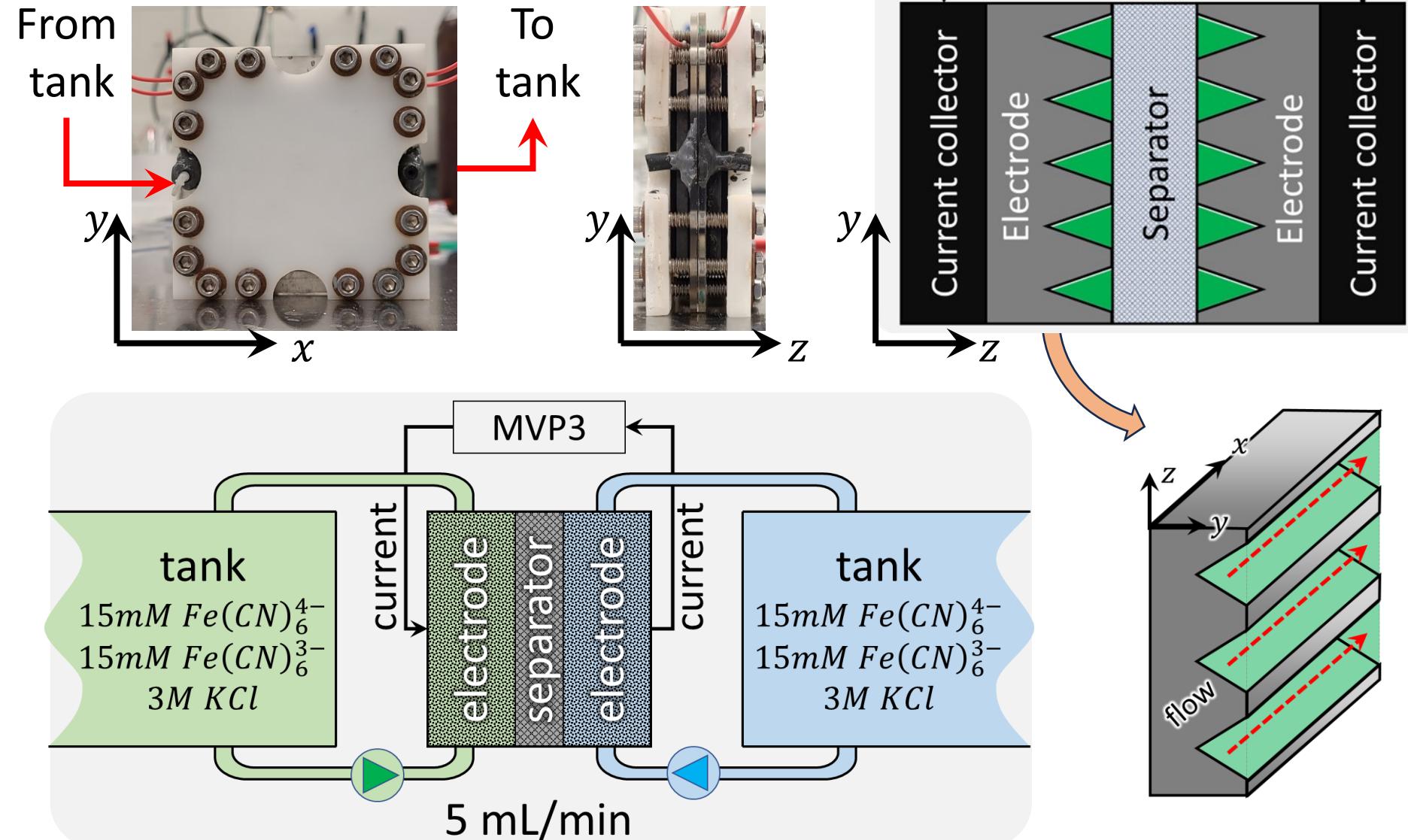
# Warburg impedance and mass transfer



$$Re \ll 1$$

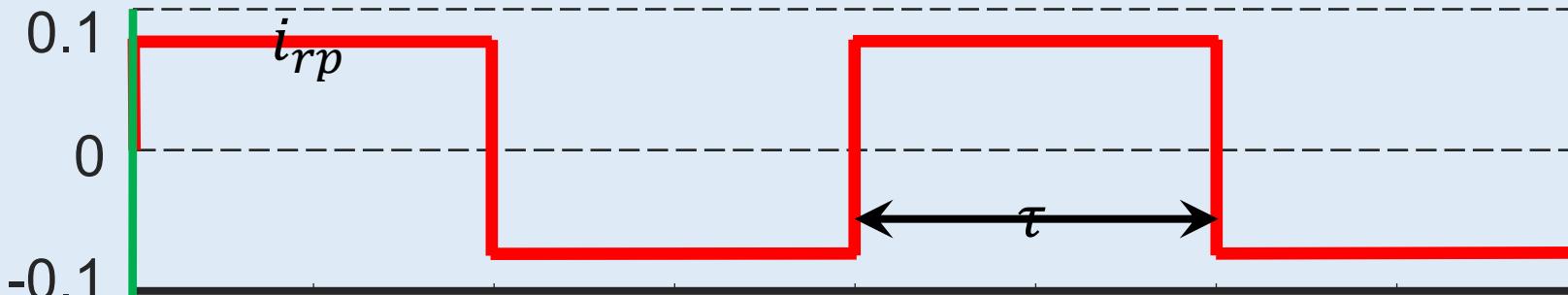
$$Pe = \frac{v l_c}{D} = \frac{\text{advection rate}}{\text{diffusion rate}} \longrightarrow Pe = Re \cdot Sc$$

# Transient experiment

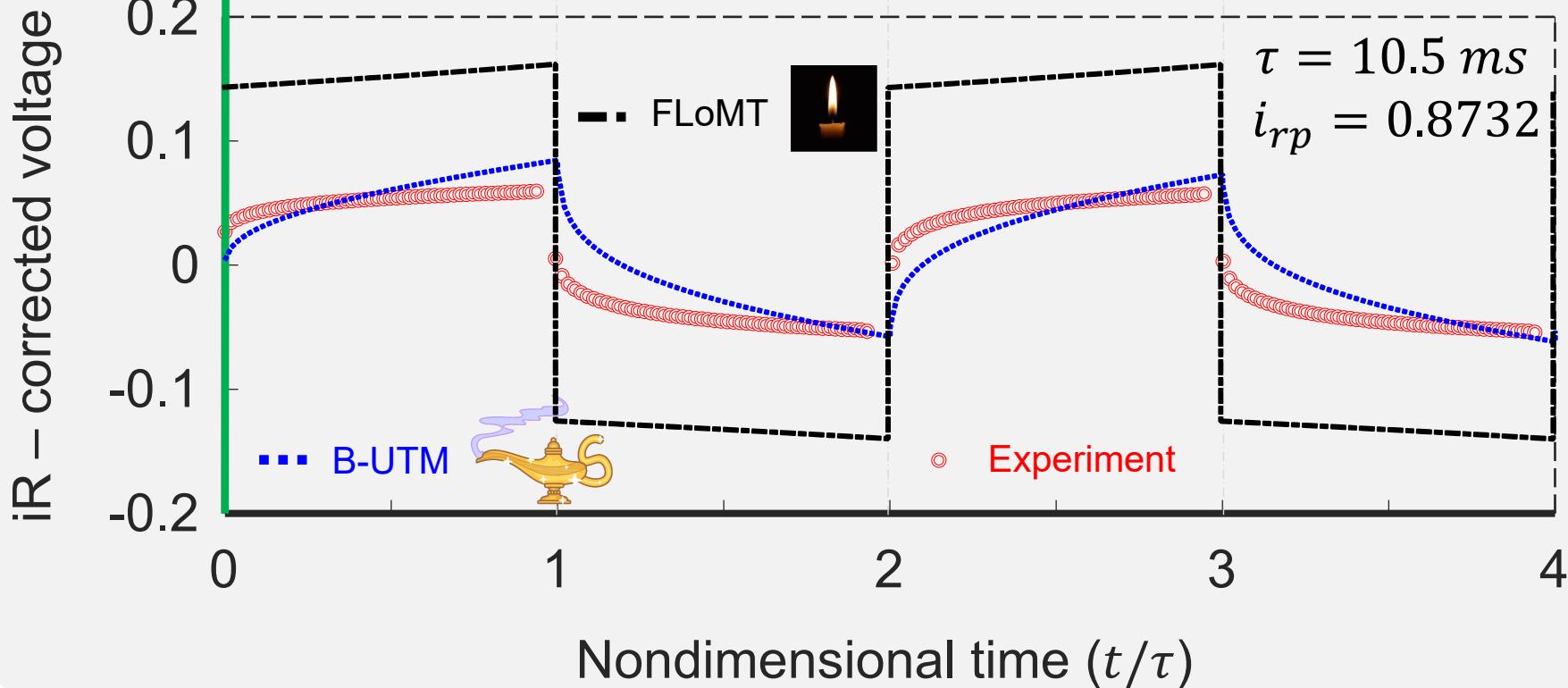


# Experiment and simulations

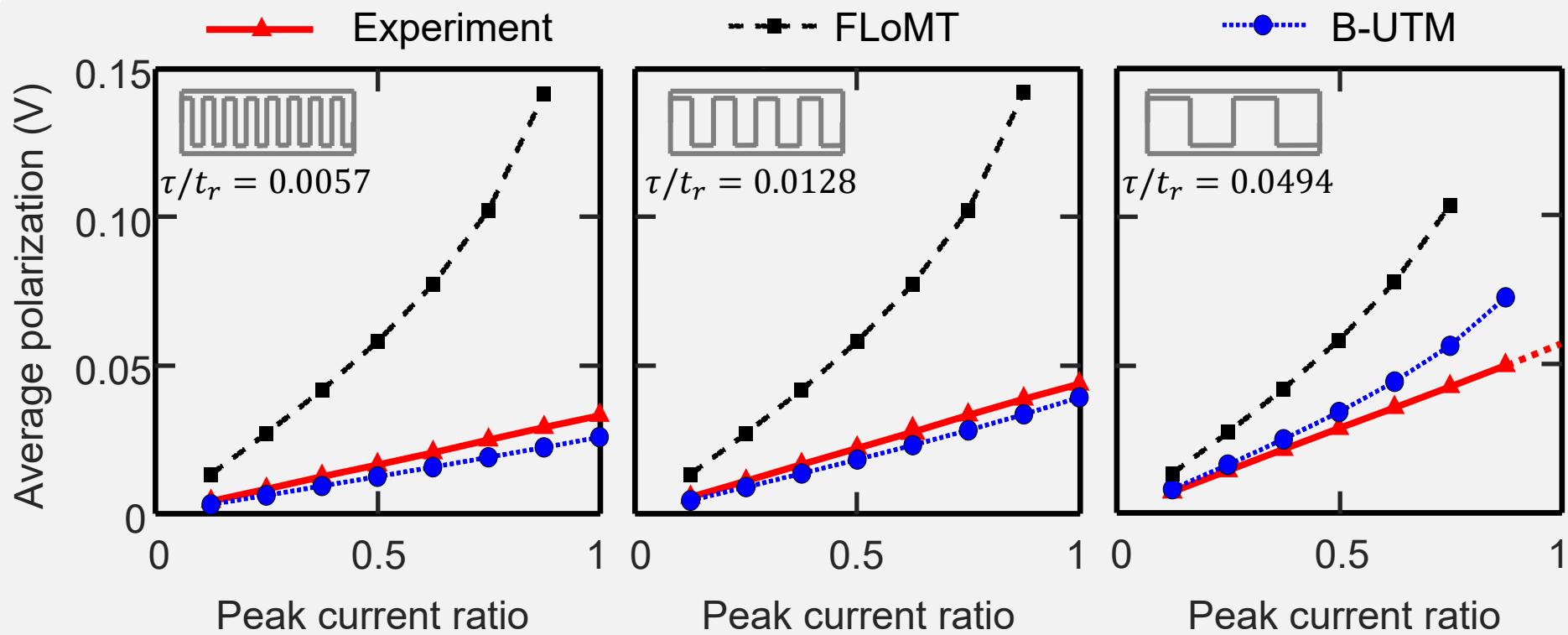
Current



$iR$  – corrected voltage



# Experiment and simulations (cont..)



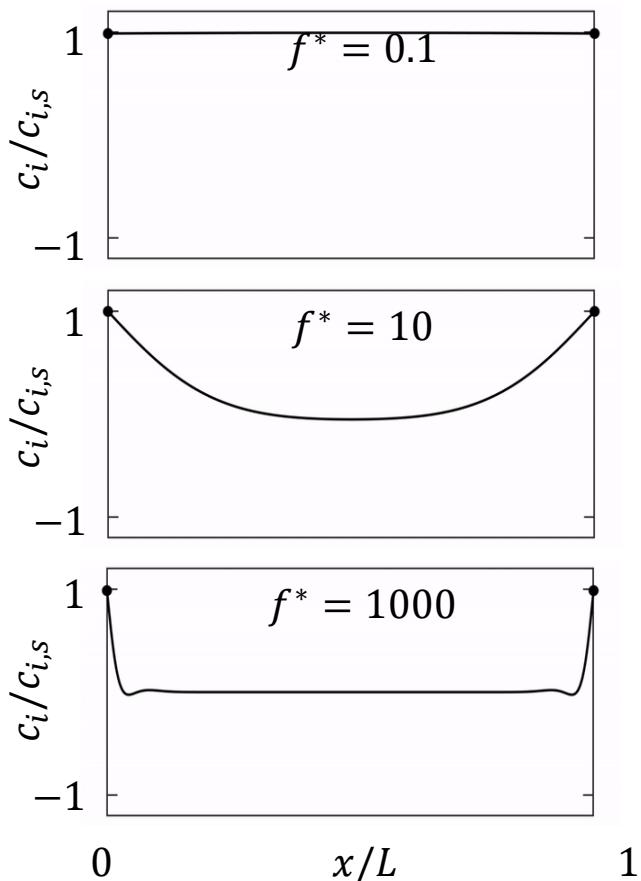
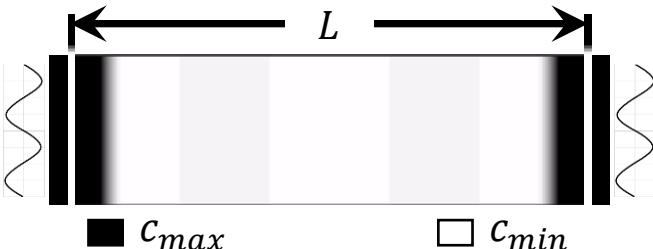
Mean residence time

$$t_r = \frac{\text{flow length}}{\text{superficial velocity}}$$

FLoMT : Up to 400% overprediction

B-UTM : Significant improvement

# Why overpredicts $\tilde{Z}_w$



- In conventional theories  the **diffusion length** is taken as constant.
- Usually the **pore dimension/size** is taken as characteristics diffusion length.
- At high frequency **actual diffusion length** decreases considerably.
- **Transient theory**  is mandatory for such high frequency operation.



# Frequency dependent pore-scale transport

$$\frac{\partial c_i}{\partial t} + \nabla \cdot (\mathbf{u}^\square c_i - D_i \nabla c_i) = 0$$

$$c_i \Big|_S = c_{i,s}(t)$$

Valid for facile reaction  
 $Da \gg \min[1, e^{\alpha \frac{F\eta}{RT}}]$

Fourier transform  
 $\mathcal{F}\{A(t)\} = \bar{A}(\omega)$

$$\nabla \cdot (\mathbf{u}^\square \bar{c}_i - D_i \nabla \bar{c}_i) + j\omega \bar{c}_i = 0$$

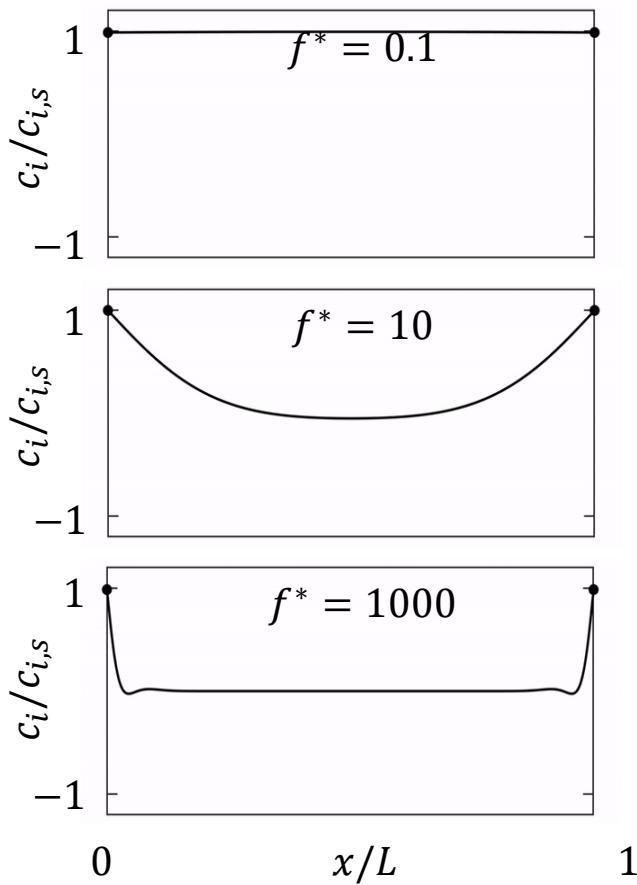
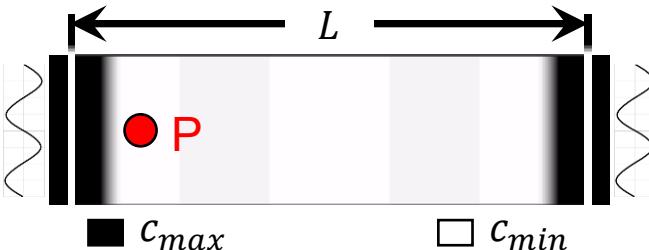
$$\bar{c}_i \Big|_S = \bar{c}_{i,s}(\omega)$$

$$\nabla \cdot (\mathbf{u}^\square \mathbb{C}_i - D_i \nabla \mathbb{C}_i) + j\omega \mathbb{C}_i = 0$$

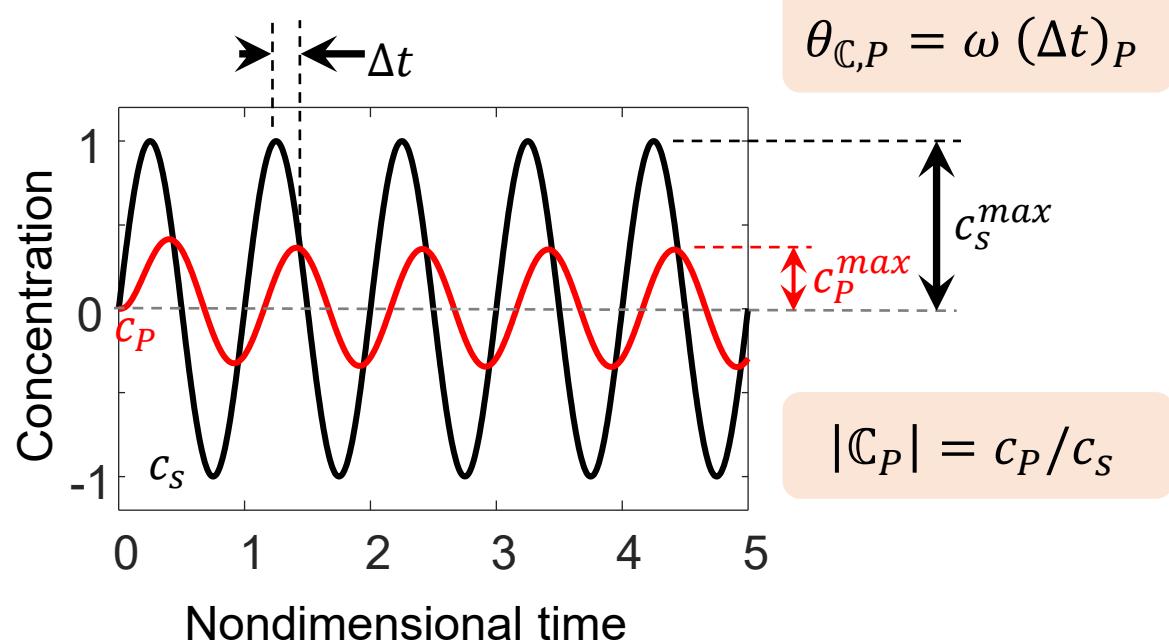
$$\mathbb{C}_i \Big|_S = 1$$

Transfer function:  
 $\mathbb{C}_i(\omega, \mathbf{r}) \equiv \frac{\bar{c}_i(\omega, \mathbf{r})}{\bar{c}_{i,s}(\omega)}$

# Transfer function $\mathbb{C}(\omega, r)$ in parallel plates



- $\mathbb{C}$  provides local transient response under pure-sinusoidal *disturbance*.
- At surface  $|\mathbb{C}| = 1$  and  $\theta_{\mathbb{C}} = 0$ .



# Volume averaged TF - Diffusion

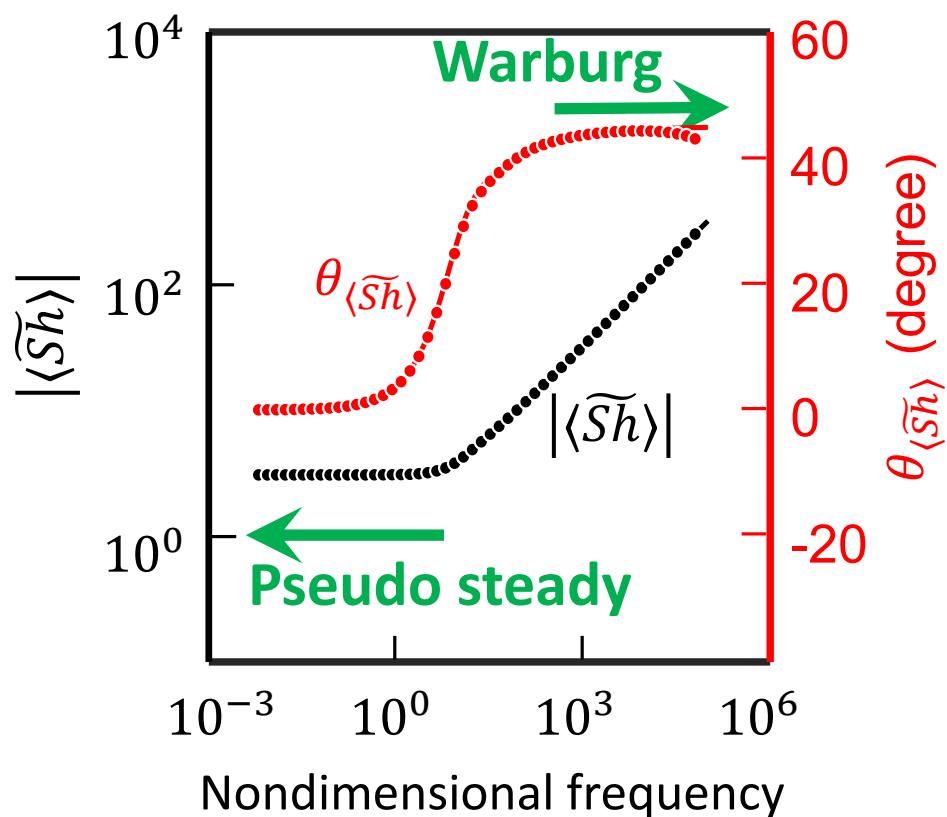
Spectral Sherwood number



$$\langle \widetilde{Sh} \rangle(\omega) \equiv \left( \frac{b}{D} \right) \frac{\langle \bar{J} \rangle_s}{\bar{c}_s - \langle \bar{c} \rangle}$$
$$= \frac{-\langle \partial \mathbb{C} / \partial n^* \rangle}{1 - \langle \mathbb{C} \rangle}$$

Gives Instantaneous reaction rate

$\langle \dots \rangle$  and  $\langle \dots \rangle_s$  are respectively integral averages over solution volume and solid/solution interfaces



# Volume averaged TF - advection

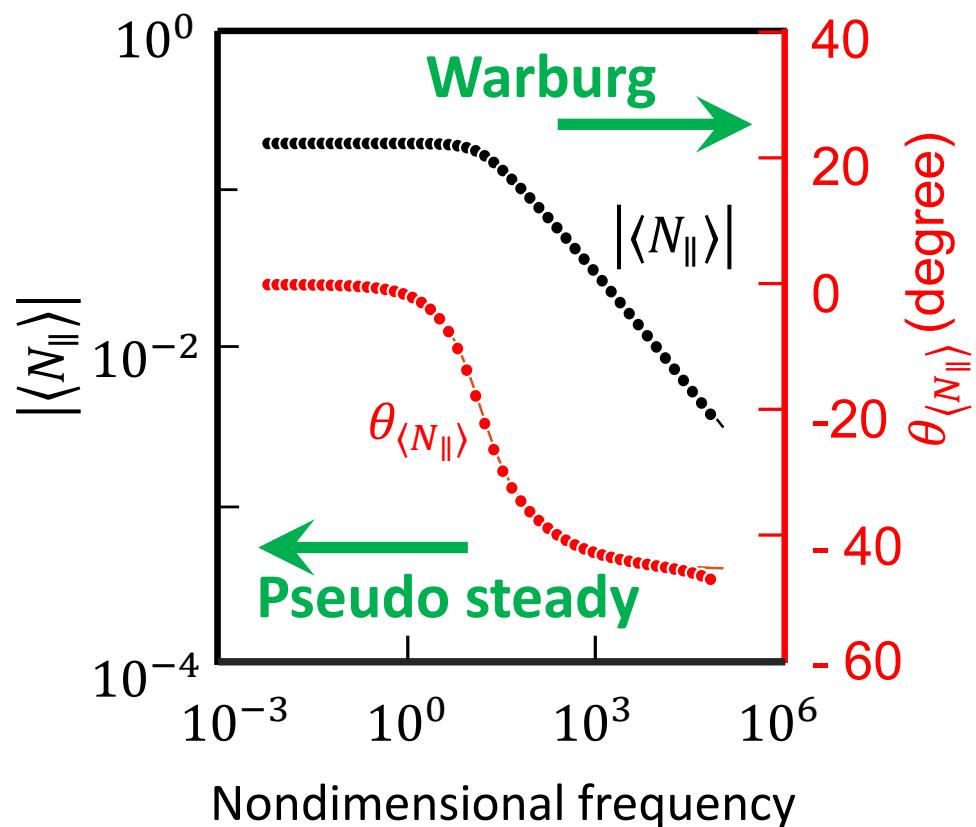
Advective-flux transfer function



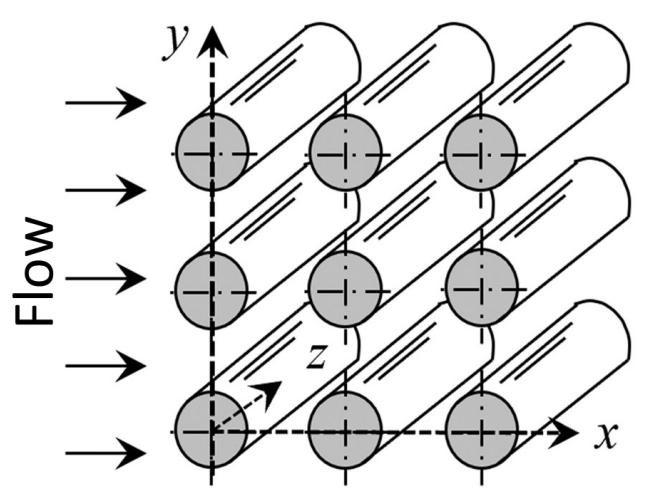
$$\langle N \rangle \equiv \left( \frac{\varepsilon}{|\mathbf{u}_s|} \right) \frac{\langle \bar{W} \rangle}{\bar{c}_s - \langle \bar{c} \rangle}$$

$$\begin{aligned}\langle W \rangle &\equiv -\text{covar}(\mathbf{u}^\square, c) \\ &= (\mathbf{u}_s / \varepsilon) \langle c \rangle - \langle \mathbf{u}^\square c \rangle\end{aligned}$$

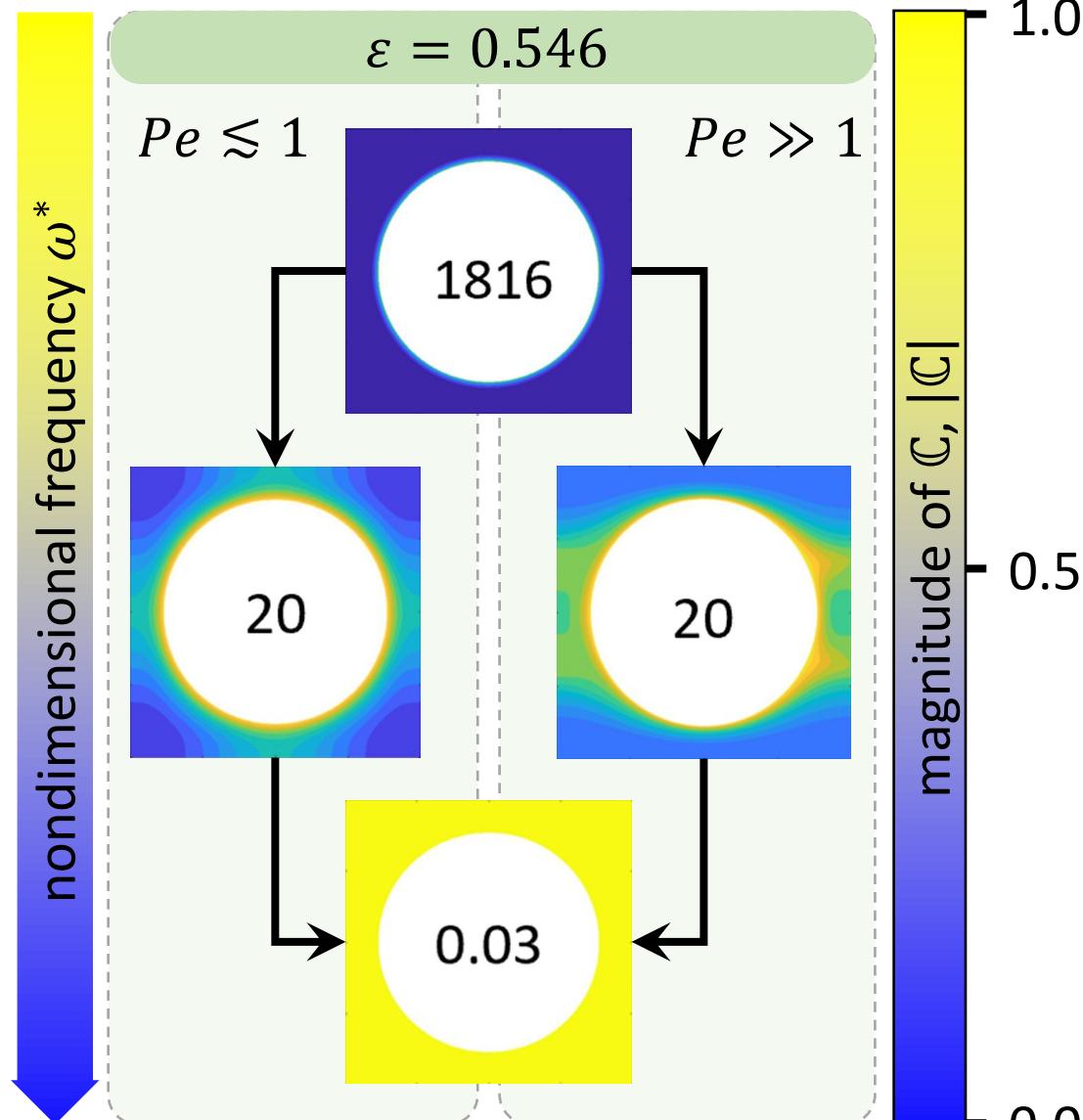
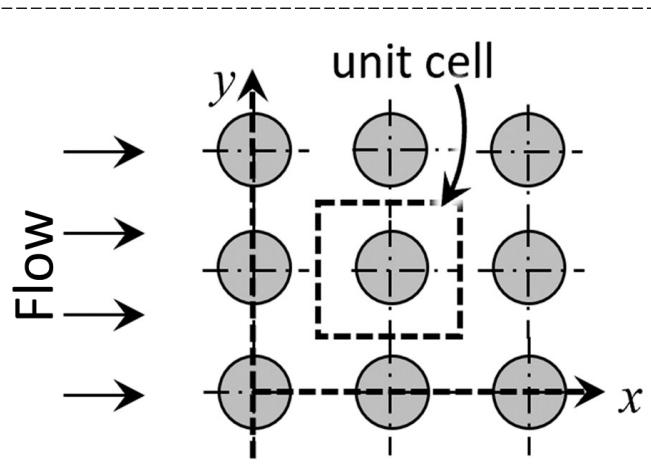
Gives  
fractional deviation in  
advection rate



# Porous electrode

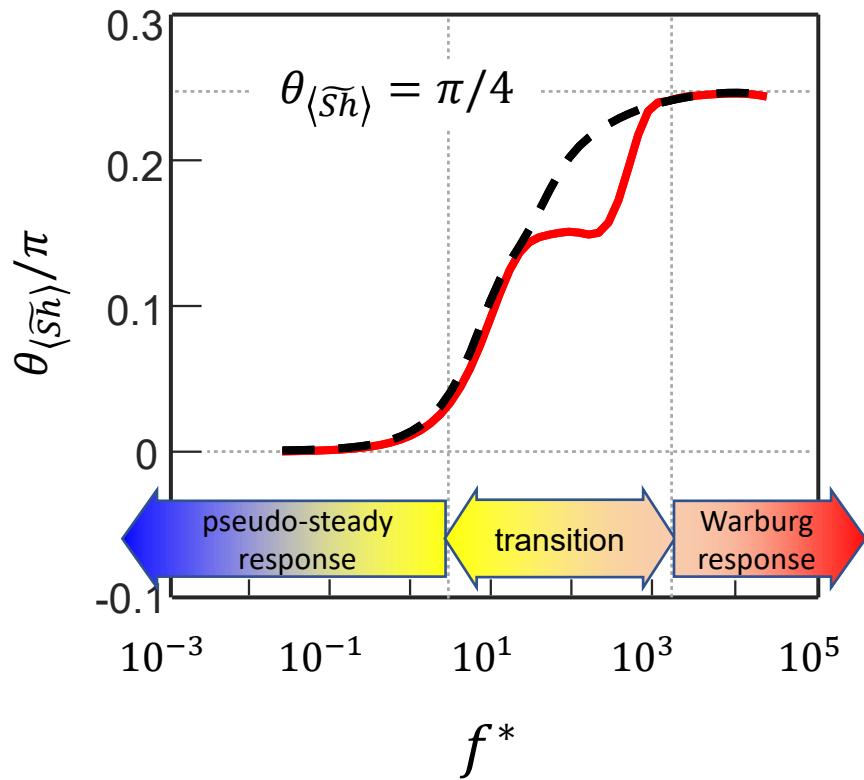
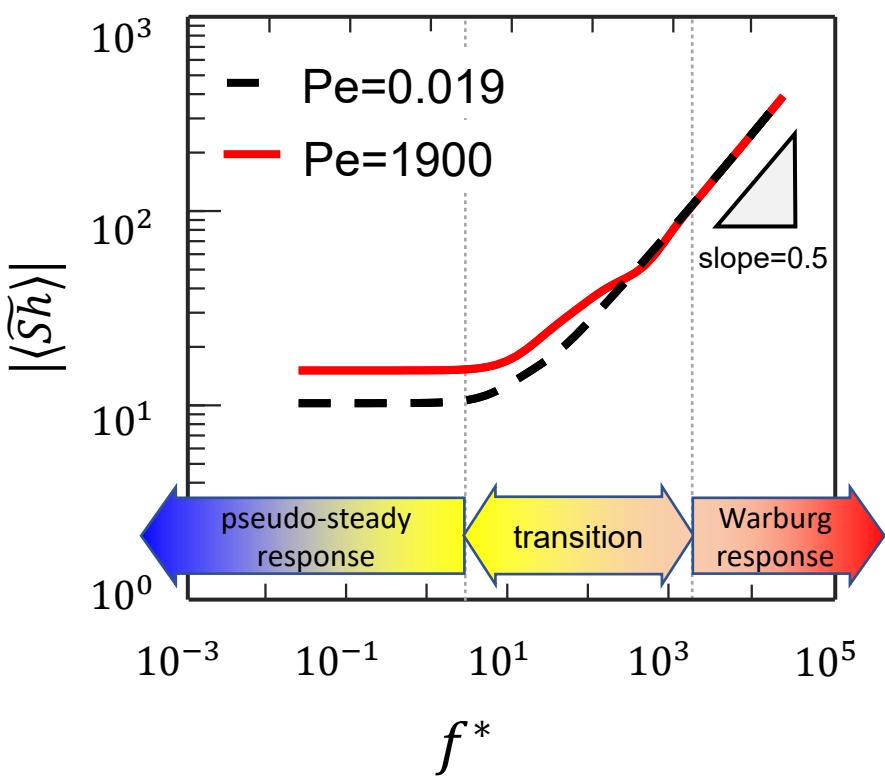


Mimics carbon fiber electrode



# Volume averaged coefficient - Diffusion

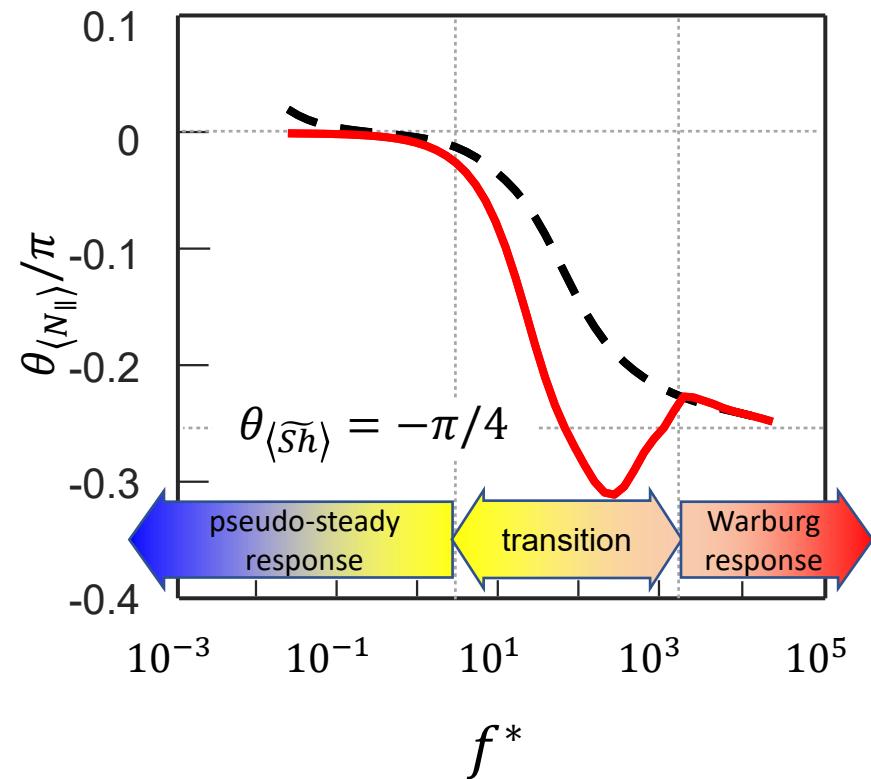
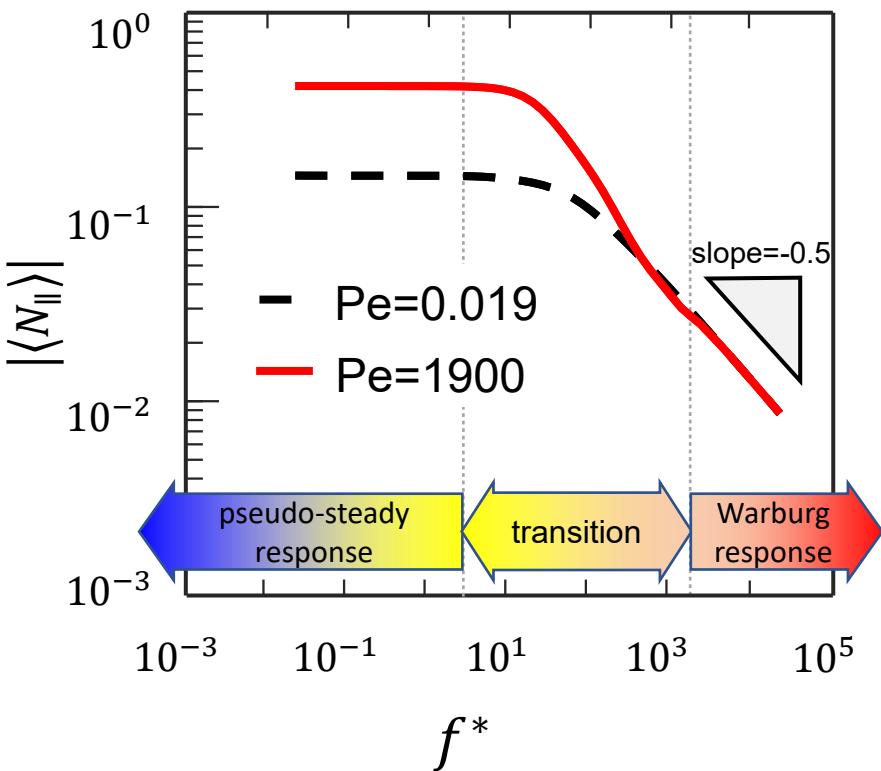
Spectral Sherwood number:  $\langle \widetilde{Sh} \rangle(\omega) \equiv \left( \frac{b}{D} \right) \frac{\langle \bar{j} \rangle_s}{\bar{c}_s - \langle \bar{c} \rangle} = \frac{-\langle \partial \mathbb{C} / \partial n^* \rangle}{1 - \langle \mathbb{C} \rangle}$



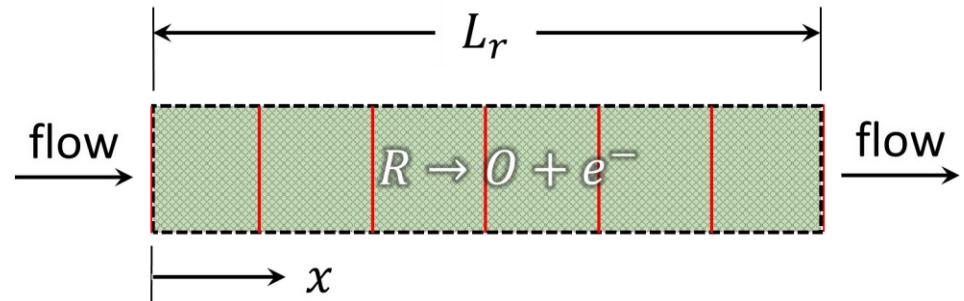
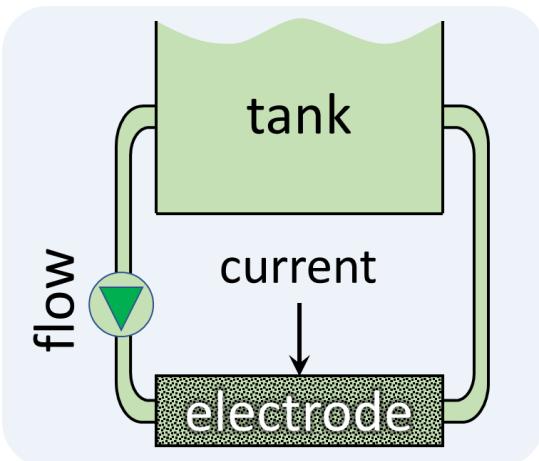
# Volume averaged coefficient - advection

Advective-flux transfer function

$$\langle N \rangle \equiv \left( \frac{\varepsilon}{|\mathbf{u}_s|} \right) \frac{\langle \bar{W} \rangle}{\bar{c}_s - \langle \bar{c} \rangle}$$



# Frequency dependent up-scaled transport



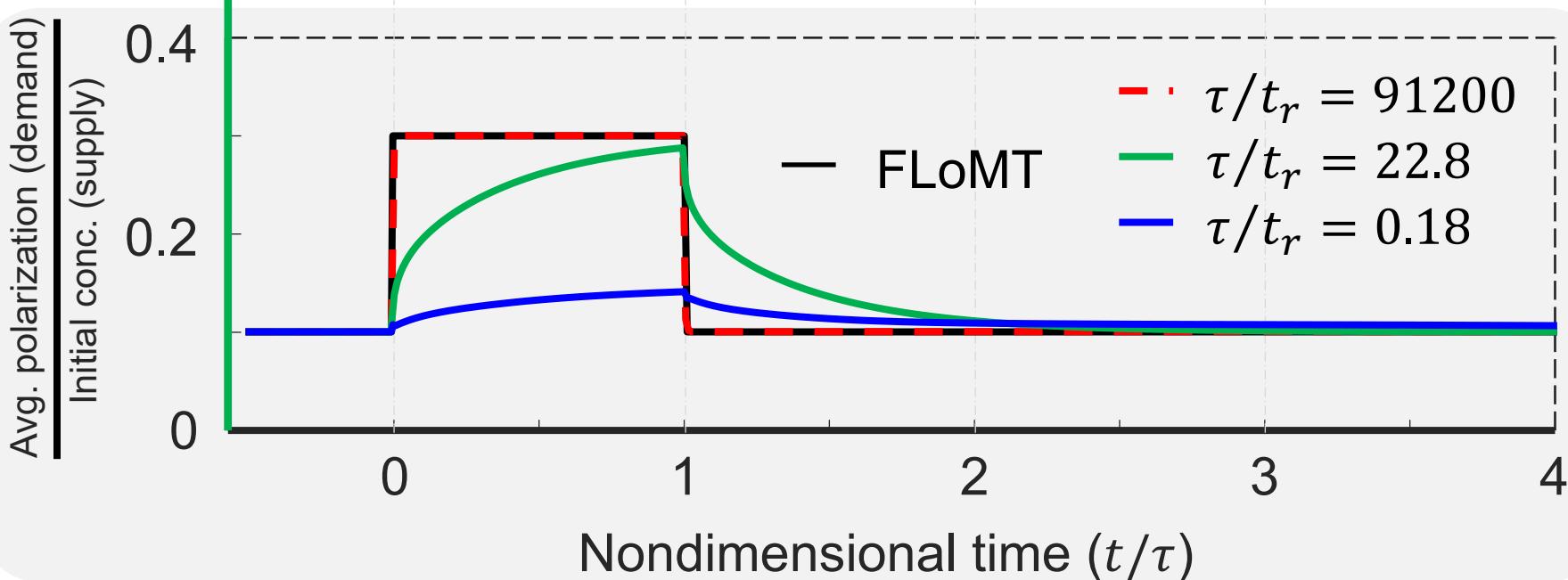
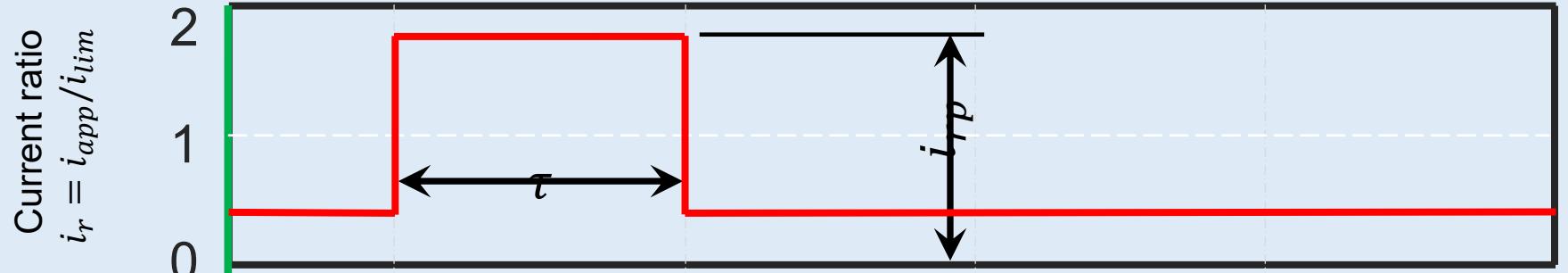
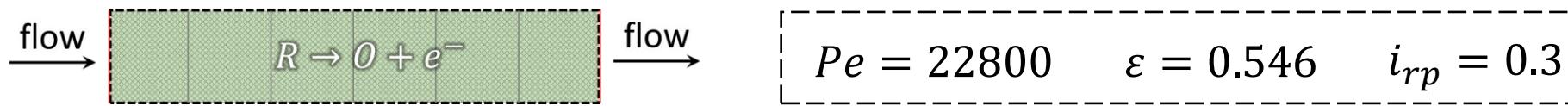
1-D upscaled model using  
porous electrode theory

$$\varepsilon \frac{\partial \langle c_i \rangle}{\partial t} + \nabla \cdot \mathbf{u}_s \langle c_i \rangle - |\mathbf{u}_s| \nabla \cdot \mathcal{F}^{-1} \{ \langle \mathbf{N} \rangle (\bar{c}_{s,i} - \langle \bar{c} \rangle_i) \} = \frac{a D_i}{s_i b} \mathcal{F}^{-1} \{ \langle \widetilde{Sh} \rangle (\bar{c}_{s,i} - \langle \bar{c} \rangle_i) \}$$

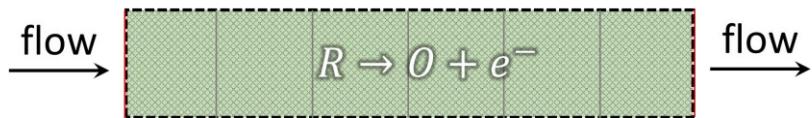
Accounts for  
instantaneous deviation  
of advection rate

Accounts for the  
instantaneous reaction  
rate

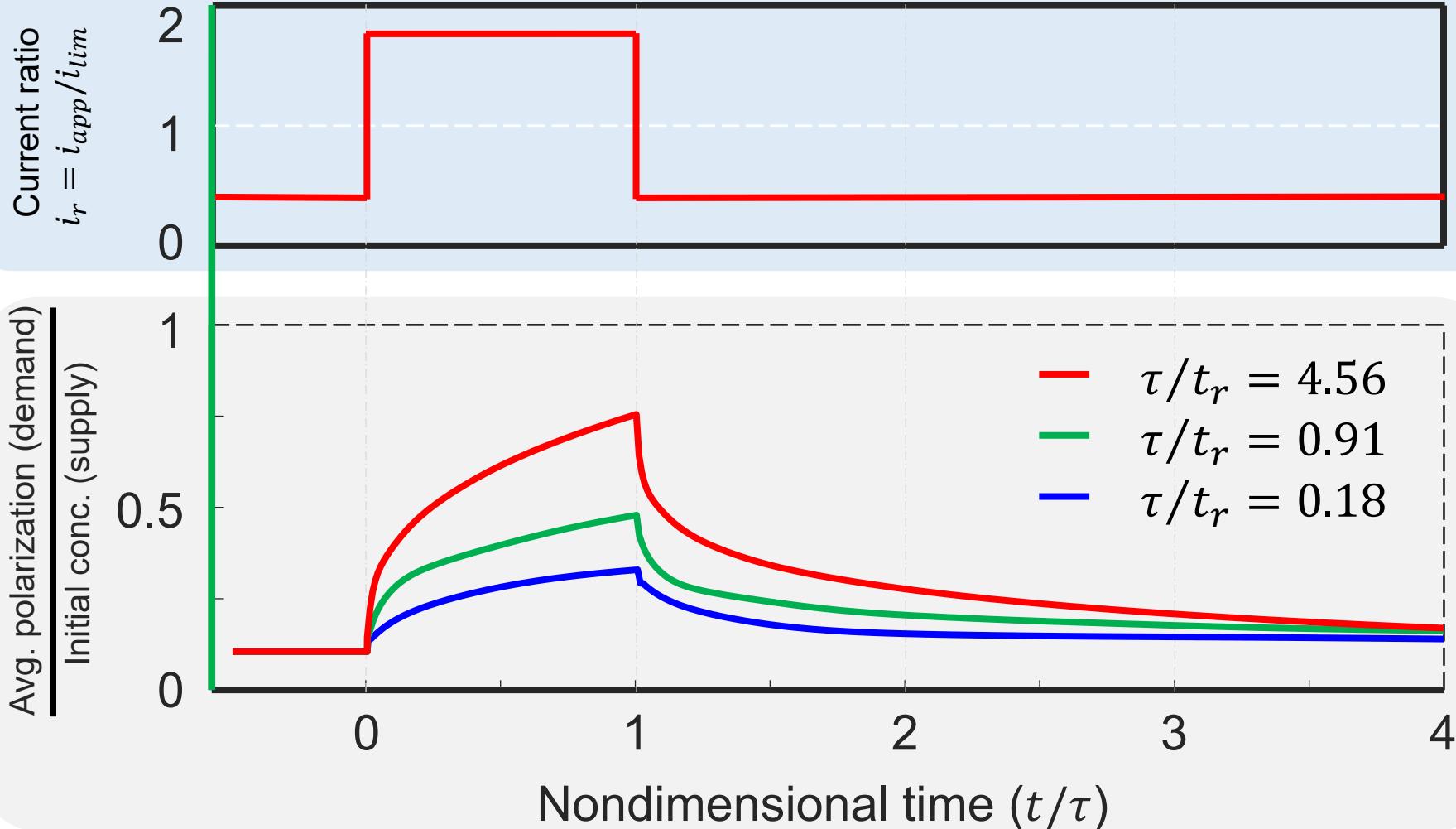
# Average polarization - reactant demand



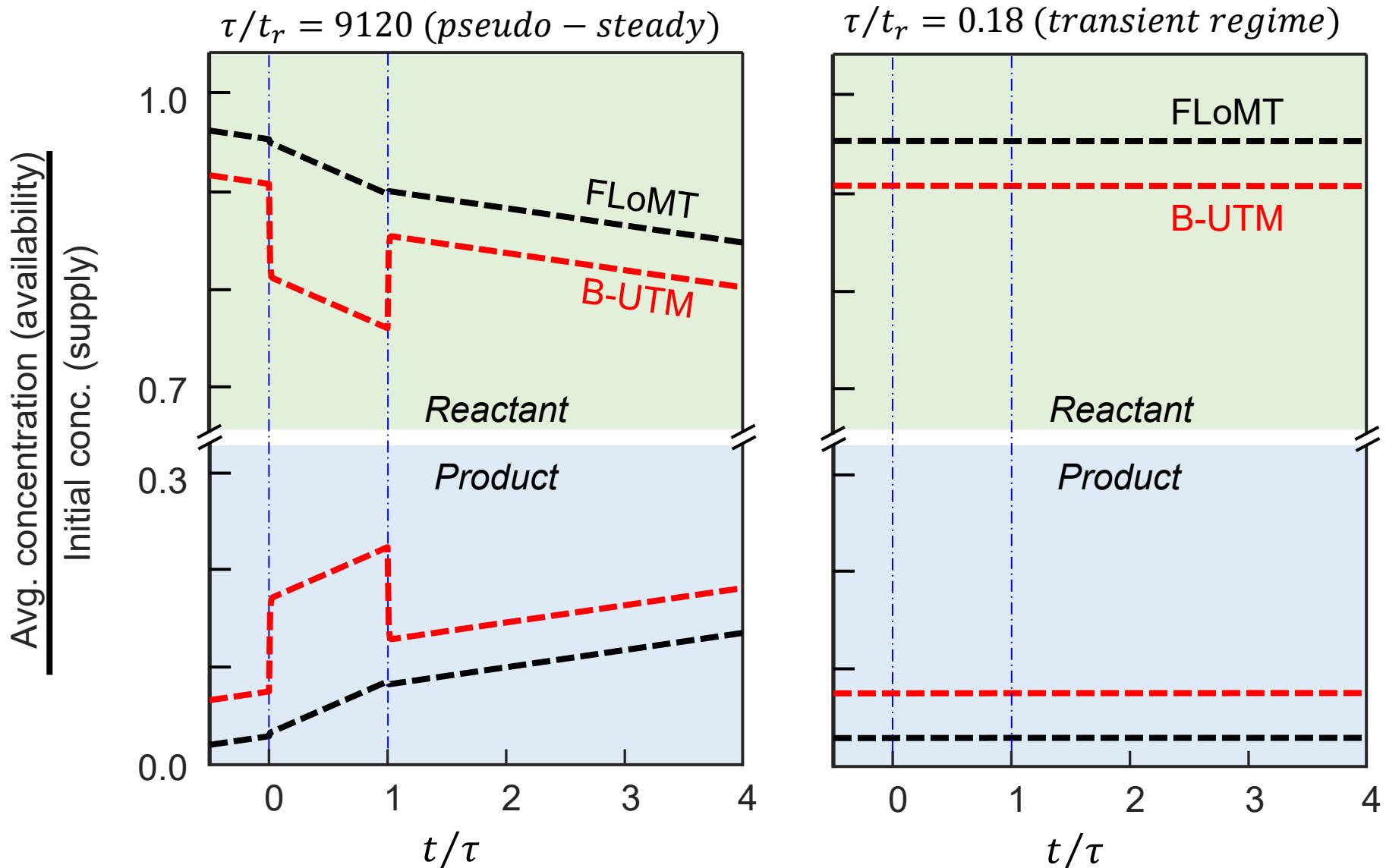
# Average polarization (over-limiting operation)



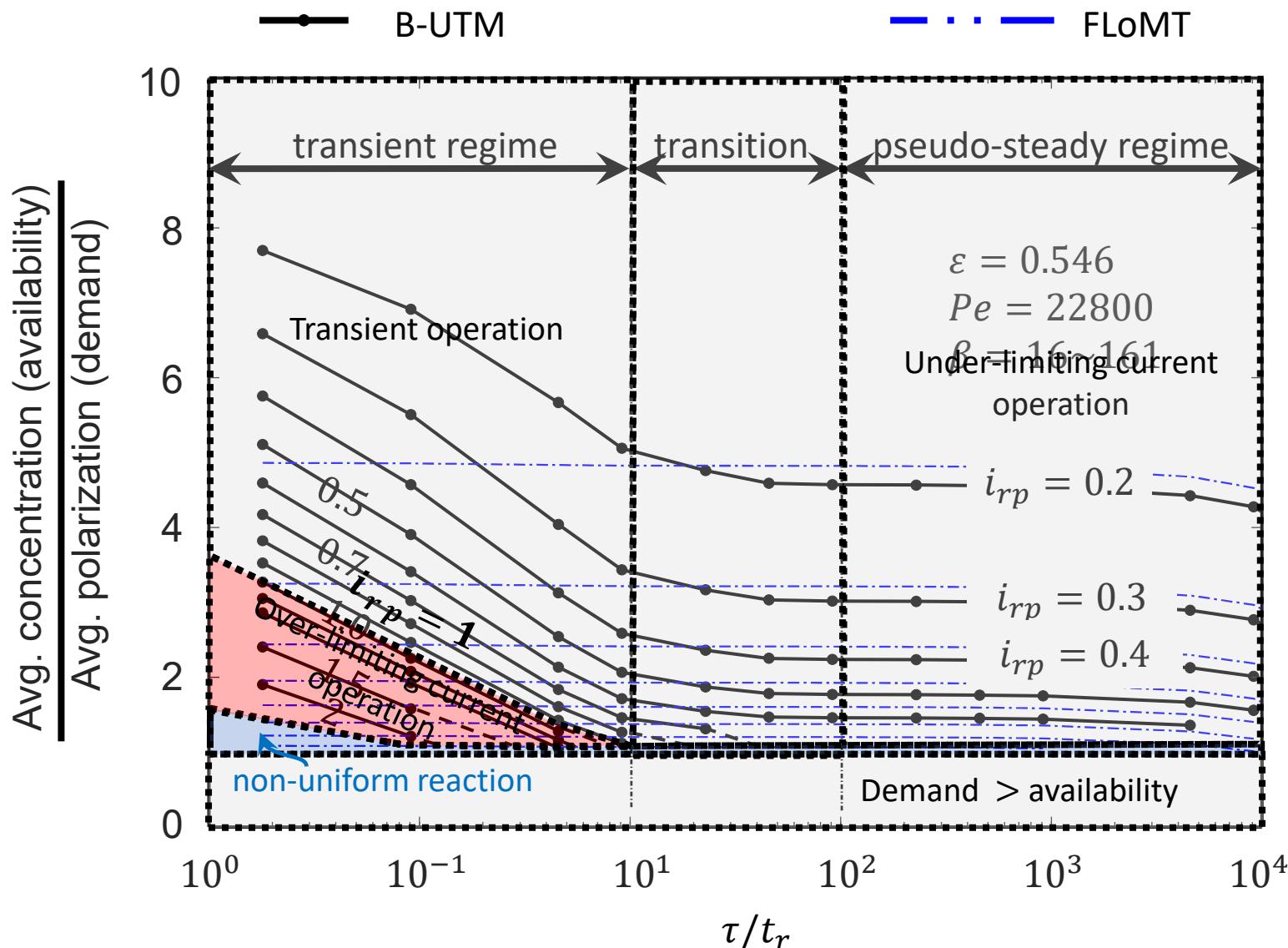
$$Pe = 22800 \quad \varepsilon = 0.546 \quad i_{rp} = 1.2$$



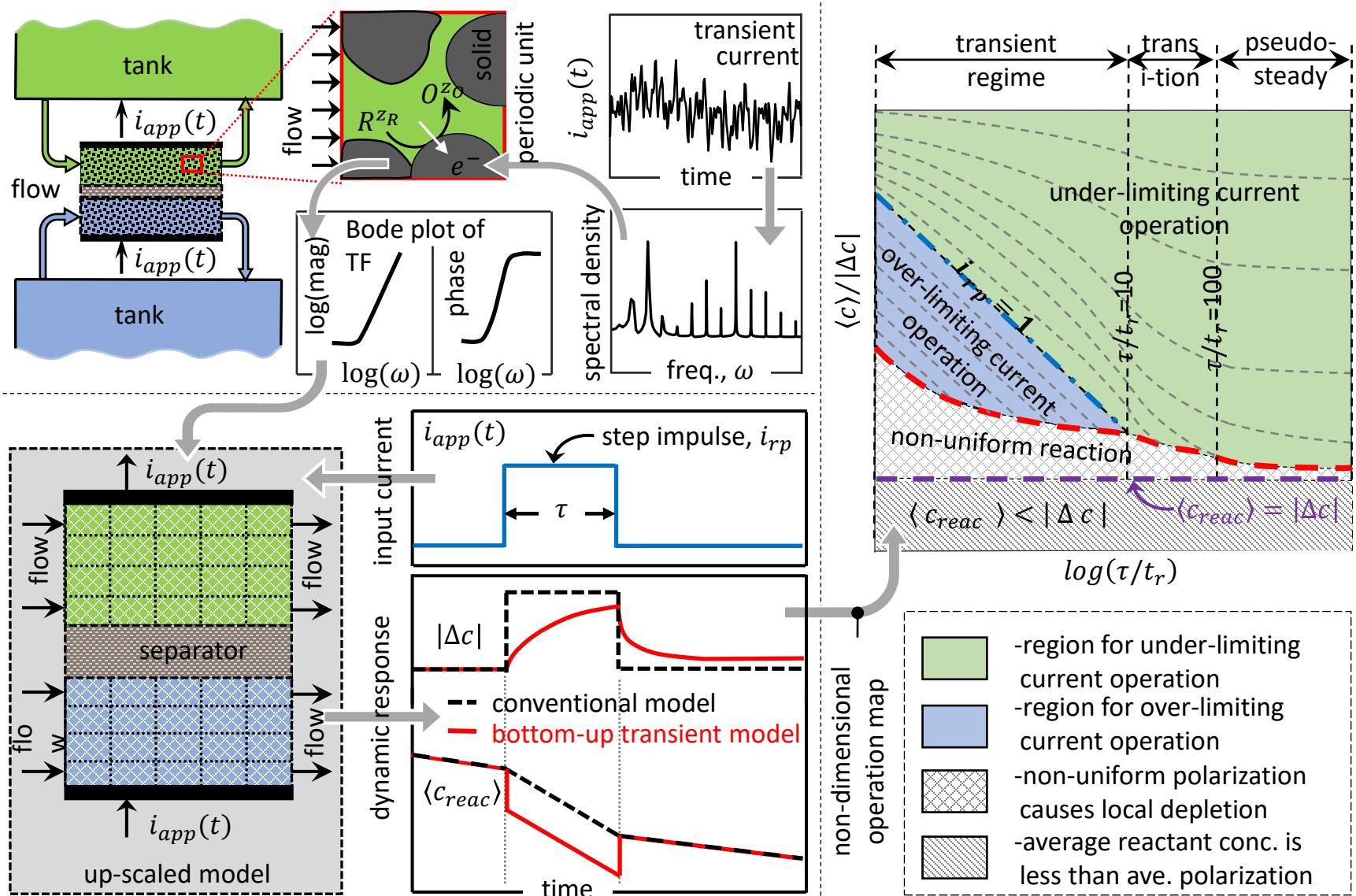
# Average concentration - reactant availability



# Non-dimensional maps of operational space

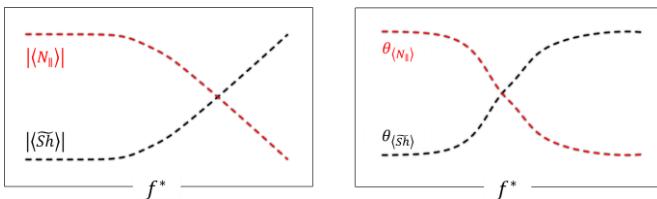
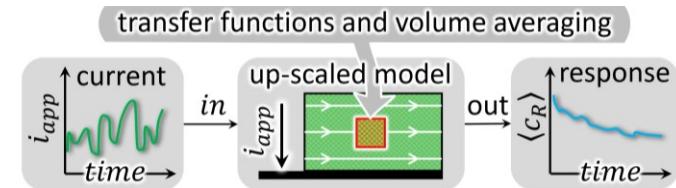


# Reviewing the theory briefly



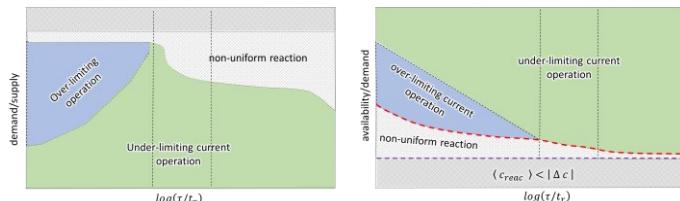
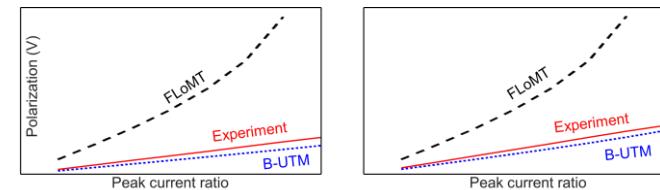
# Conclusions

A bottom-up multi-scale theory is developed which can capture transient response of FBs.



Volume averaged TFs enable direct upscaling.

Compared to FLoMT, B-UTM predictions are significantly close to experimental observations.



Over-limiting current is possible for short period of time.

